

FORMULATION AND EVALUATION OF A CHITOSAN-PVA-GELLAN INSULIN IMPLANT

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ABSTRACT

Objective: The purpose of this study was to ascertain the applicability of degradable materials for fabrication of an insulin release system.

Methods: Insulin implants were prepared by using poly (vinyl alcohol) (PVA), gellan and chitosan by solution casting method. The prepared implants were evaluated for swellability, content uniformity, potency and purity of insulin in implants, scanning electron microscopy studies, *in vitro* release studies, *in vitro* degradation studies using lysozyme, stability studies and circular dichroism spectroscopy.

Results: The swelling degree of the implants was found to be in the range of 1.07-1.56. The diffusion coefficient of water through the implant was found to depend on the calcium chloride (CaCl₂) concentration. The diffusion coefficient of insulin through the chitosan-PVA-gellan in the early stages was found to be in the range of 1.99×10^{-5} cm²/sec to 5.24×10^{-5} cm²/sec and at later stages in the range of 6.9×10^{-6} cm²/sec to 1.10×10^{-5} cm²/sec. The weight of the implants was 48 ± 0.58 mg. The insulin content in the implants was 9.86 ± 0.10 mg. The potency of insulin extracted from the implants was 27.11 ± 0.75 U/mg or 95.12 ± 2.61 % of the control insulin. The *in vitro* release studies showed that insulin was released completely in a period of 13-19 d depending on the composition of the implant. The increase in CaCl₂ retarded the rate of insulin release whereas the increase in PVA content leads to the rapid release of insulin. The device was found to undergo significant weight loss due to enzyme mediated degradation.

Conclusion: These studies provide validity for the potential utility of chitosan-PVA-gellan implant systems for the delivery of insulin. The studies also demonstrate that insulin maintained its integrity within the implant system. Implants showed the complete release of insulin in 19 d and the release of insulin from the implants depended on the amount of CaCl₂.

Keywords: Insulin, Degradation, Diffusion, Gellan, Chitosan

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INTRODUCTION

Diabetes mellitus refers to a group of metabolic diseases characterised by chronic hyperglycemia, due to defects in insulin secretion. The treatment of diabetes by insulin injection provides only a poor approximation of normal glucose homeostasis, especially for insulin-dependent diabetes where blood glucose concentrations vary widely despite insulin therapy [1, 2]. This is because the pharmacokinetics of insulin following subcutaneous injection does not match the profiles of physiological insulin secretion [3, 4]. Moreover, subcutaneous injections result in localized insulin deposits that lead to local hypertrophy and fat deposits under the skin. Together these disadvantages lead to suboptimal pharmacodynamics properties of the applied insulin, which does not allow mimicking the complex physiological insulin secretion pattern [5].

Polymeric implants are one of the promising devices for protein drug delivery. Some polymeric matrices can protect drugs from physiological conditions that could degrade the proteins. Therefore, a lot of research is ongoing to identify appropriate polymer systems to formulate ideal protein drug delivery systems that would allow ease of incorporation of protein drugs without affecting their bioactivity, deliver them at the desired rate and exhibit biocompatibility when in contact with the tissue [6]. Gellan is an anionic polysaccharide of microbial origin, which is capable of forming a three-dimensional network by complexation with cations and hydrogen bonding with water. The apparent viscosity of gellan gum dispersions can be markedly increased by increasing both pH and cation concentration [7]. Furthermore, its ingestion has never produced reported adverse dietary, physiological or toxic effects in animals and humans. These properties make this polysaccharide suitable for several commercial applications, such as in the food industry and in drug delivery [8]. While gellan gum has never been used to deliver biologically active macromolecules, it has some potential for this application. The ion-induced cross-linking property of gellan avoids the presence of initiator or organic cross-linker that can be toxic to the protein activity if not removed from the device. The preparation also does not need to involve organic solvents and/or high temperatures that could

denature the protein. Polyvinyl alcohol (PVA) is one of the hydrogels often used in biomedical applications [9]. It is a water-soluble synthetic polymer with excellent film forming, emulsifying and adhesive properties. Chitosan forms a polyionic complex with gellan and this property was used in the current work to prepare an insulin implant of chitosan-PVA-gellan for maintenance of prolonged therapeutic levels of insulin.

The objective of this investigation was to develop a chitosan-PVA-gellan implant device as an implant for insulin delivery. The procedure for the preparation of chitosan-PVA-gellan implant was optimized. The swelling index and *in vitro* release characteristics for drug delivery were investigated.

MATERIALS AND METHODS

Materials

Gellan, polyvinyl alcohol (average molecular weight range 1,20,000–1,80,000 and degree of hydrolysis 99%), Chitosan (medium molecular weight, 75-85% deacetylated), insulin (porcine pancreas) were purchased from Sigma, St. Louis, MO, USA. Lysozyme (HiMedia 50,000 U/mg), Calcium chloride (CaCl₂), potassium dihydrogen phosphate, sodium hydroxide and sodium chloride were obtained from SISCO Scientific Laboratories, Mumbai India.

Preparation of chitosan-PVA-gellan insulin implant

The compositions of various formulations are given in table 1. A 0.5% w/v chitosan solution in 0.2 M acetic acid was poured into a glass mold (Area 28.3 cm²) and dried at 25 °C under vacuum for 48 h. PVA was dissolved in water by heating to 90 °C, to which gellan and glycerin (2% v/v) were added and stirred until a clear solution was obtained. To this solution, insulin dissolved in small volume of 0.1 N HCl and diluted with pH 7.4 phosphate buffered saline (PBS) was added at 25 °C and stirred gently [9]. The solution was then poured over the chitosan film in a glass mould and dried at 25 °C under vacuum for 24 h. Over this layer 10 ml of 0.5%, w/v of chitosan was poured and was allowed to dry at 25 °C under vacuum. The dry formulations were cut into 10 mm circular discs.

Table 1: The composition of various formulations

Ingredients	F-I	F-II	F-III	F-IV
Gellan (% w/v)	1	1	1	1
Poly(vinyl alcohol) (% w/v)	3	3	6	6
Glycerin (mL)	3	3	3	3
CaCl ₂ (%w/v)	0.05	0.1	0.05	0.1
Distilled water (mL)	20	20	20	20

Content uniformity, potency and purity of insulin in implants

Content uniformity and insulin potency in the implants was determined by an RP-HPLC method (Shimadzu LC 10 AD, Japan). The implants were reduced to small pieces and placed in 20 ml of 0.05 N HCl for 24 h and filtered using Whatman filter paper. From this 0.1 ml was pipetted out into a 10 ml standard volumetric flask and made up to the volume with 0.05 N HCl and assayed for drug content by reversed-phase high-performance liquid chromatography method (RP-HPLC). The RP-HPLC consisted of the C-18 column; the mobile phase was 0.2 M sodium sulphate (pH 2.3) and acetonitrile in the ratio of 74:26. The flow rate was 1 ml/min and the insulin was detected using UV detector at 214 nm [10].

The potency of insulin was calculated from the relationship:

$$C_u = \frac{C_s R_u}{R_s}$$

Where C_u is the potency of the unknown, C_s : is standard potency, R_u : peak area of unknown and R_s : peak area of the standard [11].

Swelling studies

Implants were placed in a glass beaker containing 50 ml of phosphate buffered saline (PBS, pH 7.4) and the beakers were placed in a shaking incubator at 37 °C and 100 rpm. The implants were weighed periodically throughout the experiment. The swelling process was characterised by the swollen weight ratio ($q = W_s/W_d$), where W_s is the weight of the swollen implant and W_d is the weight of the initial dry implant. The swelling studies were carried out in triplicate. The Berens-Hopfenberg equation [12] was fitted to the data obtained from the swelling studies.

$$\frac{M_t}{M_\infty} = \{1 - A \exp(-k_2 t)\} \quad (1)$$

where A and k_2 are constants calculated from the slopes and intercepts of the plot of $\log(1 - M_t/M_\infty)$ versus time t at times later than those corresponding to $M_t/M_\infty = 0.6$. The equation $M_t/M_\infty = kt^n$ adequately describing a major portion of the swelling behaviour fails to give an accurate analysis above $M_t/M_\infty = 0.6$. To obtain a better model after 60%, we have used Berens-Hopfenberg equation.

Scanning electron microscopy studies

The surface morphology of dried implants was determined using a scanning electron microscope (JEOL 6320). The implant samples were mounted on a base plate and coated with gold using a vapour deposition technique. The surface was then scanned at magnifications of 500× and 1000×.

In vitro release studies

The implant was placed in 100 ml glass beaker containing 50 ml of PBS (pH 7.4). The beaker was placed in a shaking incubator at 37 °C and 100 rpm. The samples were withdrawn every 24 h and the insulin concentration was determined using RP-HPLC. The *in vitro* release studies were carried out until the complete release of insulin was observed.

Mathematical analysis of water uptake and drug release

Analysis of the swelling behaviour of implants in PBS at pH 7.4 was carried out using the equation.

$$\frac{M_t}{M_\infty} = 1 - \frac{8}{\pi^2} \exp\left(-\frac{\pi^2 Dt}{4\delta^2}\right) \text{ for } 0.4 < M_t/M_\infty < 1 \quad (2)$$

Where D is the water diffusion coefficient, δ the half thickness of the implant, M_t the amount of water uptake at the time, t and M_∞ is the water uptake at equilibrium [13]. Diffusion coefficients of insulin through the implants were calculated with Eqs. 2 and 3:

$$\frac{M_t}{M_\infty} = 4 \left(\sqrt{\frac{Dt}{\pi\delta^2}} \right) \text{ for } 0.4 < M_t/M_\infty < 1 \quad (2)$$

Where D is the insulin diffusion coefficient, δ the half thickness of the implant, M_t the amount of insulin released at the time, t and M_∞ is the amount of insulin in the implant. Equation 3 was used to calculate the diffusion coefficient of insulin at early stages when the fraction of insulin released (M_t/M_∞) was less than 0.6 and for later stages equation 2 was used when the fraction of insulin released (M_t/M_∞) was greater than 0.6. This is because plotting with equations 2 and 3 fits the experimental data well until $M_t/M_\infty < 0.6$.

Enzyme-mediated degradation studies

The implants were placed in 10 ml phosphate buffer (pH 7.4, 37 °C) containing lysozyme enzyme (1 mg/ml). The PBS was changed for all the samples every day. Implants were taken out at 7, 14, 21 and 28 d, washed with distilled water and air-dried for 72 h. The resulting dry weights were recorded. The mass loss of the samples was determined by gravimetry.

Stability studies

The stability protocol was based on the International Conference on Harmonisation (ICH) 'Q1A (R₂)' guidelines. The implants were stored at 25 ± 2 °C and 60 ± 5 % RH for and at 5 ± 3 °C which is the accelerated storage temperature and long term storage temperatures respectively, for products intended to be refrigerated. Stability studies were performed for e formulation F2. The stability testing of samples was carried out at 0, 60, 120 and 180 d under long-term storage conditions. For accelerated conditions, the samples were assayed every 10 d for 30 d.

Circular dichroism spectroscopy

Circular dichroism (CD) spectra were obtained with a Jasco J-810 spectropolarimeter (Japan) equipped with a Peltier temperature controller. Spectra were collected at 20°C using a 0.1 cm cell over the wavelength range of 200–270 nm. A resolution of 0.1 nm and scanning speed of 10 nm/min with a 2 s response time were employed. Each spectrum obtained represents an average of three consecutive scans. Noise reduction, blank buffer subtraction, and data analysis were performed using standard analysis and temperature/wavelength analysis programs (Jasco). Secondary structure content was estimated employing CDPPro software with data in the range of 200–240 nm using the basis 4 and 7 programs for input data. Loaded implants containing insulin were dialyzed against water at 4 °C for 24 h before analysis by CD. Standard insulin solutions were prepared at 0.1 mg/ml in 10 mmol PBS.

RESULTS AND DISCUSSION

Content uniformity, potency and purity of insulin in implants

The disc implants were 48 ± 0.58 mg and had a thickness 851 ± 8.9 μm. The insulin content in the implants was 9.86 ± 0.10 mg. The potency of insulin extracted from the implants was 27.11 ± 0.75 U/mg or 95.12 ± 2.61 % of the control insulin. There was no significant difference ($p < 0.001$) in potency or purity of the insulin extracted from implants compared to that of standard insulin. In addition, after storage at 2–8 °C for 6 mo, insulin in the implants manifested the same potency and purity as the initial preparation.

Swelling studies

Primarily three mechanisms could be responsible for the release of drugs from the hydrogels: swelling, diffusion and degradation. Upon exposure to an aqueous media, first, the polymer swells due to the uptake of the water. The rate of water uptake by the implant depends on the hydrophobicity of the polymer. Second, when the implant swells, the encapsulated drug is released by diffusion through the pores formed due to swelling. The third mechanism, which involves degradation of the polymer matrix, would occur under *in vivo* conditions as a result of enzyme activity.

The effect of crosslinking agents on the swell ability of the polymer could be demonstrated by the diffusion coefficient of water in the implant system. Moreover, the rate of drug delivery from an implant also depends on the rate of diffusion of the water front into the device. It is known that the greater the molecular size/weight of the drug, the greater is the sensitivity of the diffusion coefficient to changes in crosslink density. Insulin is regarded as a macromolecular peptide whose release from the implant apparently depends on the diffusion coefficient of water in the device as well as on the swellability of the polymer.

The swelling degree of the implants was found to be in the range of 1.07-1.56. The Berens-Hopfenberg differential equation $\frac{M_t}{M_\infty} = \{1 - A \exp(-K_2 t)\}$ was fitted to the data obtained from the swelling studies to assess the overall kinetics governing the swelling.

Table 2: Parameters A, k_2 and diffusion coefficient of water from swelling studies

Formulations	A	$k_2 \times 10^{-3} (\text{min}^{-1})$	R^2	D (cm^2/sec)
F1	0.25	3.1	0.992	2.08×10^{-4}
F2	0.17	2.6	0.973	1.73×10^{-4}
F3	0.43	5.3	0.986	2.28×10^{-6}
F4	0.28	6.5	0.991	2.18×10^{-6}

(n=3) mean±SD

Scanning electron microscopy studies

The scanning electron microscopy studies of the PVA/gellan implants (fig. 1 and 2) clearly showed a difference in the microstructure of the swollen and dry state of the cross section of the implant. This provides structural proof for the hypotheses we made regarding the release of insulin from the implant systems due to swelling of the polymer.

In vitro release studies

The formulation F1 showed the complete release of insulin in 16 d, while for F2, F3 and F4 complete release of insulin were seen in 19, 13 and 15 d respectively. Obviously, this infers that the release depends on the PVA content and CaCl₂ concentration in the formulation. The increase in CaCl₂ retarded the rate of insulin release whereas the increase in PVA content leads to rapid release of insulin. The *in vitro* release of the various formulations is shown in the fig. 3. The fraction of insulin released (M_t/M_∞) less than 0.6 was fitted to the equation $M_t/M_\infty = k t^n$, where M_t is the insulin released at time t , M_∞ is the maximum insulin released, k is the characteristic constant of the polymer, and n is the characteristic exponent describing the penetration mechanism. For planar geometry, a value of $n=0.5$ indicates a Fickian diffusion mechanism, $0.5 < n < 1.0$ indicates non-Fickian or anomalous transport, and $n=1$ implies case II (relaxation controlled) transport. The constants n and k were calculated from the slope and intercepts of the plots of $\log (M_t/M_\infty)$ versus $\log t$, respectively. The calculated value of n was 0.86-0.89, which indicated that the release of insulin followed non-Fickian or anomalous transport. This suggests that the release of insulin from the implant was controlled by swelling of the matrix due to water penetration into the implant.

The diffusion coefficient of insulin (molecular weight 5900, hydrodynamic radius 16 \AA) was calculated using Eqs.2 and 3 (table 3). The diffusion coefficient of insulin decreased when the concentration of CaCl₂ increased due to an increase in the crosslink

In this equation, M_t is the swelling at time t and M_∞ is the equilibrium swelling. In this studies, the constants A and k_2 were calculated from the slopes and intercepts of the plot of $\log(1 - M_t/M_\infty)$ versus time t at times later than those corresponding to $M_t/M_\infty = 0.6$. The calculated values of A and k_2 are listed in table 2. The values of A were in the range of 0.17-0.43 indicating Fickian diffusion. The diffusion coefficient for water transport was calculated by plotting $\log [\pi^2/8(1 - M_t/M_\infty)]$ versus t for $0.4 < M_t/M_\infty < 1$ (Eq. 2). The slope of the plot was $\pi^2 D/2.303 \times 4\delta^2$ from which the diffusion coefficient D was calculated (table 2). The diffusion coefficient of water through the implant was found to depend on the CaCl₂ concentration.

The maximum diffusion coefficient was observed with implants prepared with a CaCl₂ concentration of 0.05% w/v. When the cross linker concentration was increased from 0.05% w/v (F1) to 0.1% w/v (F2) the diffusion coefficient of water through the implant decreased from 2.08×10^{-4} to $1.73 \times 10^{-4} \text{ cm}^2/\text{sec}$ and from 2.28×10^{-6} to $2.18 \times 10^{-6} \text{ cm}^2/\text{sec}$ for F3 and F4, respectively. This may be explained by the fact that on increasing the crosslinker content there is a prominent decrease in the free volumes available between the chains of the macromolecular network and thus the swelling of implant decreases. The crosslink density of hydrogels provides a restricted aqueous environment for diffusional migration of the peptide, by controlling both the degree of hydration and the permeability of hydrogels to protein [14].

density, which compacts the network. It is likely that the increase in the compactness restricts the mobility of the network chains (chain relaxation) and impedes diffusion of insulin from the implant.

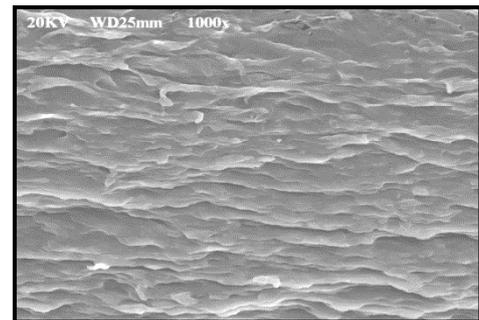


Fig. 1: SEM pictures of cross-section of implant (F2) before swelling

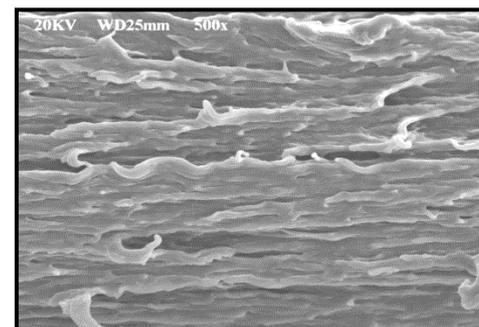


Fig. 2: SEM pictures of cross-section of implant after swelling (F2) in a buffer medium over a period of 240 min

Table 3: Diffusion coefficients of insulin through the implant

Formulations	Diffusion coefficient ($\times 10^{-5} \text{ cm}^2/\text{sec}$)	
	Early stages	Later stages
F1	6.65	0.92
F2	3.33	0.69
F3	8.73	1.10
F4	7.85	0.77

(n=3) mean \pm SD

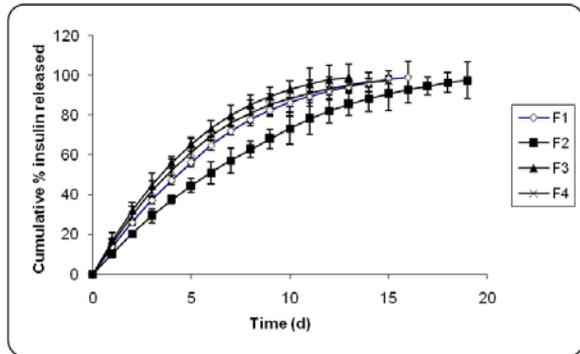


Fig. 3: *In vitro* release studies of insulin implants in PBS (7.4) at 37 °C, n=3, Data presented as mean \pm SD

Enzyme-mediated degradation studies

It is known that chitosans with block structures and lower degrees of deacetylation (<75%) are more readily degraded due to the presence of blocks of glucosamine moieties containing acetyl groups that serve as a substrate for lysozyme. In the present study, we used chitosan (75-85% deacetylated) that has been shown to degrade *in vivo* in about 6 mo [15].

The *in vitro* degradation studies showed that there was a significant weight loss of the implants when placed in phosphate buffer solution pH 7.4 containing lysozyme indicating the degradation of the implants. The degradation studies were carried out for 4 w and the % weight loss of the implants was found to be 20.8 \pm 2.0 (fig. 4).

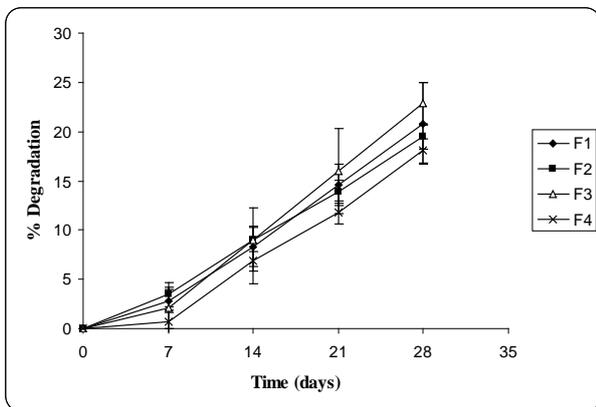


Fig. 4: Degradation studies of the implants F1, F2, F3 and F4, n=3, Data presented as mean \pm SD

Stability studies

Observations under long-term storage conditions and accelerated conditions are shown in the fig. 5 and 6. The insulin content in the formulation in long-term storage conditions and accelerated storage conditions along with 95% confidence limits were plotted (sigmaplot® version 9.0). When the implants were stored under long-term storage conditions the insulin content in formulation F2

was found to be 9.47 \pm 0.06 mg (94.7% of the initial content) after six mo. Under accelerated conditions, the insulin content was 7.50 \pm 0.23 mg (75% of the initial content). These results suggest that at any time (either during transit or storage) the insulin implants should be stored at refrigerator temperatures.

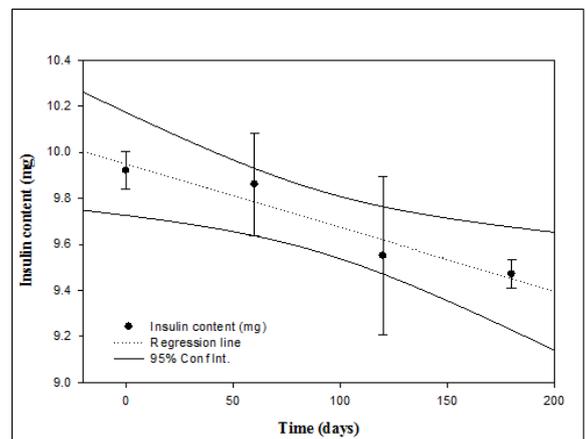


Fig. 5: Insulin content in the implants (F2) when stored at 5 \pm 3 °C for 180 d, n=3, Data presented as mean \pm SD

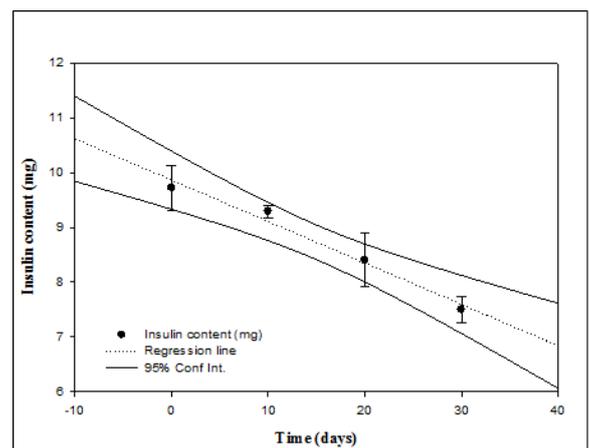


Fig. 6: Insulin content in the implants (F2) when stored at 25 \pm 2 °C and 65%RH \pm 5%RH for 30 d. n=3, Data presented as mean \pm SD

Circular dichroism spectroscopy

The CD spectra of control insulin and the insulin extracted from the implant (F2) are shown in fig. 7.

Compared with the CD spectrum of control insulin, no significant change was observed in that of the insulin extracted from the implant in the PBS solution, indicating that the conformation of insulin remained unchanged in the implants.

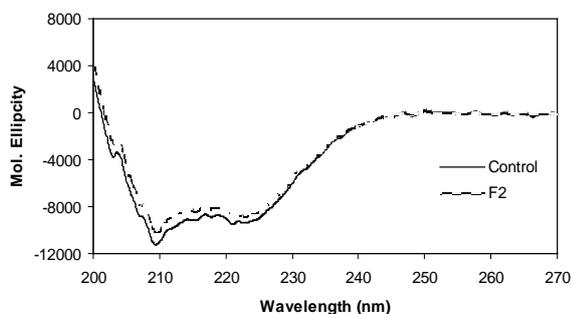


Fig. 7: The CD spectra

CONCLUSION

These studies provide validity for the potential utility of chitosan-PVA-gellan implant systems for the delivery of insulin. The studies also demonstrate that insulin maintained its integrity within the implant system. Implants showed the complete release of insulin in 19 d and the release of insulin from the implants depended on the amount of CaCl_2 . Further investigations to prolong the release of insulin over longer durations will be undertaken.

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CONFLICTS OF INTERESTS

Declare none

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