

Original Article

OPTIMIZATION OF ALBENDAZOLE 400 MG TABLET COMPRESSION PROCESS USING DESIGN OF EXPERIMENT (DOE) APPROACH

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ABSTRACT

Objective: The present study aims to model and optimize the compression process of the Albendazole 400 mg tablets of a pharmaceutical industry production line to increase the production speed (tablets/h) while maintaining quality requirements.

Methods: The study was conducted using the Design of Experiments (DoE) methodology to identify and correlate the critical parameters during the process that affect the maintenance of the compression speed. In order to support the experiments, was tested disintegration time, average hardness, hardness variation, average weight, and friability.

Results: Was obtained that quality attributes of disintegration and friability did not generate a significant model but it has been established correlations between Fill-O-Matic speed and main compression force in the responses of weight variation, hardness, and mean hardness. It was found that the main compression force between 6 to 9 kN, the pre-compression force of 1,965 to 5,615 kN, and the speed of 55 RPM for Fill-O-Matic speed are responsible for ensuring that all quality attributes analyzed remain within the expected specification.

Conclusion: It was possible to apply the Design of Experiment (DoE) methodology in the compression process of the drug Albendazole 400 mg and to evaluate the impact of the parameters of this step on the formation of the tablet to significantly increasing the productivity of this product. The Fill-O-Matic speed parameter was the main control factor discovered in this study to maintain quality attributes.

Keywords: Design of Experiment, Tablets, Press machine, Fill-O-Matic speed, Fette

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INTRODUCTION

The tablet is the most consumed and produced pharmaceutical form in the world. This fact is possibly justified by the greater chemical stability of the tablets when compared to other dosage forms. Besides that, they are more convenient to handle and are mostly administered orally. Also, tablets can be produced on a fast and extremely reproducible industrial scale, with highly controlled quality attributes [1].

The compression process used in the manufacture of tablets is given by the literal compression of a quantity of powder within the die cavity of a tablet press machine. The procedure is basically divided into 3 sub-steps: die cavity filling, tablet production with punches moving within the die, thereby compressing powder into the desired tablets (compression), and ejection of the tablet. Even though it looks like a simple process, today's tablet press machines provide a huge range of parameters in order to increase process control and, in turn, enable the production of tablets at a high speed [1, 2].

When evaluated individually, the compression stage has a direct influence on some quality attributes required for a tablet, such as disintegration and dissolution times, hardness, friability, and mean weight. Thus, a more detailed study on this process is justified to maintain the quality, safety, and efficacy of the medication, while not ignoring the pharmaceutical industry's constant search for increased productivity [2, 3].

However, during the development of a drug, it is common to focus more on defining the formulation than on the parameters to be used in unit operations. It is not uncommon to encounter problems when transferring technology (Scale-up), since the formulation is often defined on a laboratory scale and aiming to meet specific quality attributes while ignoring factors such as productivity. In addition to the fact that regulatory agencies are progressively increasing the requirements for registration and post-registration of medicines, the use of a statistical-based approach in the development or re-development of a product brings greater security and robustness to the production routine and reduces the need for any eventual change in the production process [4, 5].

In this context, agencies and institutions such as the Food and Drug Administration (FDA) and International Council for Harmonization (ICH), have been publishing guides and regulations that encourage the application of the Design of Experiments (DoE) concept and, using it, to implement the statistical methodology of response surface analysis, in order to provide the pharmaceutical industry with ways to obtain greater knowledge about their products, leading to the development of more robust and reproducible processes. In ICH 8, published in 2009, it is already possible to find information on design space or "workspace", where ranges of production parameters and/or characteristics of the raw material are tested, correlating them with impacts on quality attributes. In this way, it is possible to know which variations our process is capable of withstanding so that the finished product still remains approved in the quality control tests [5, 6].

The application of DoE is important to discover the individual and/or combined influence of the changed parameters. In recent years, there has been an increasing amount of literature showing the applicability of this statistical methodology in the pharmaceutical industry [7-11] and, more specifically, in the compression stage [12-16]. In the work of Garlapati and Roi (2017), using statistical modeling, the authors were able to define the tablet press regulation parameters that best met the quality attributes of Levocetirizine tablet formulation [17]. Iancu *et al.* (2016) performed a similar series of experiments on Diclofenac Sodium orodispersible tablets to find the compression force that provided the best friability, disintegration time, wetting time, and hardness values [18].

Therefore, the purpose of this investigation was, using the Design of Experiment (DoE) methodology, to model and optimize the compression stage of the granulate produced by wet way of the Albendazole 400 mg in the form of chewable tablets. Albendazole is the newest carbamate in the benzimidazole group. The drug is indicated mainly for intestinal nematodes and cestodes. Such a product has a global presence, being one of the most used drugs for the treatment of parasitic infections [19].

In a pharmaceutical industry located in southern Brazil, the compression stage of this antiparasitic is time-consuming. The maximum validated compressing speed is about 10 RPM. Assessing the productive records of this medicine, it was found that, during previous tests aiming at increasing the compression speed, problems arose such as the variation in weight and hardness, both exceeding the control and specification limits. This study, therefore, set out to assess the effect of compression phase parameters to increase the production speed (tablets/h) while maintaining quality requirements.

MATERIALS AND METHODS

Experimental design

Design-Expert version 7.1.3 software was used for the experimental design and statistical analysis [20]. Using ICH 8, 9, and 10 as a base, we have defined the following parameters for controlling the

compression: Fill-O-Matic (FOM) Force Feeder Speed, Pre-Compression, and Main Compression forces. As response variables, the so-called quality attributes necessary for process control in the compression stage; the following attributes were used: Friability, Disintegration Time, Hardness, Relative Hardness Variation, and Weight Variation.

To assess the compression parameters influence on the response factors, we used an experimental 2³complete factorial design (CFD) plus 3 central points, resulting in a total of 11 experiments. The ranges of the parameters as well as the response factors used for both experiments are shown in table 1. During the test, the compression speed was kept constant, at 63 RPM. The significance of the model and the tested factors were calculated using Analysis of Variance (ANOVA) statistical methodology with a significance level of 95% [21].

Table 1: Values of the parameters and response variables used in the compression stage

Compression parameters	Ranges			Quality attributes	Desired response
	-1	0	1		
Fill-O-Matic Speed	25 RPM	40 RPM	55 RPM	Friability	<1,5 %*
Pre-compression Force	1,965 kN	3,79 kN	5,615 kN	Disintegration Time	<1800 s*
Main Compression Force	3,0 kN	6,5 kN	10 kN	Hardness	09-15 kp
				Relative Hardness Variation	<practicable
				Weight Variation	<5%

(*) Brazilian Pharmacopoeia [22]

Materials

The inputs used were: Lactose (Friesland Campina DMV Bv), Talc (SKC Inc), Corn Starch (Cargill Agrícola SA), Saccharin Sodium (Tiankin North Food Co, Inc), Magnesium Stearate (Itacel Fardoquímica Inc), Microcrystalline Cellulose (Itacel Fardoquímica Inc), Sodium Amidoglycolate (Itacel Fardoquímica Inc), Povidone 30 (Ashland Speciality Ingredients), Croscarmellose Sodic (Itacel Fardoquímica Inc), Micronized Albendazole (Punjab Chemical and Crop Protection), Sodium Laurilsulfate (Volp Inc) and Aerosil (Evonik Degussa Brasil Inc). The necessary materials, as well as the equipment used to manufacture the tablets, were provided by the company. The proportions were omitted because it is an industrial secret.

Dry mix

The ingredients were weighed and then sieved using a 1.5 mm mesh sieve. The inputs, already sieved, were mixed in the High Shear Comasa RD edition for 4 min with the impeller at 80 RPM.

Granulation

The agglutinating solution for granulation was prepared by adding the inputs from that stage to the water under constant agitation of the mechanical stirrer (IKA RW 20) at 300 RPM. After the ingredients are completely dissolved, was added the prepared solution to the dough under mixing with the impeller at 80 RPM. At the end of the addition, the chipper was activated at 3000 RPM for 2 min to standardize the granulate formed.

Drying

Drying was carried out in the Comasa RD Developer fluidized bed. The inlet temperature used was 50 °C. The process took about 40 min until the granules reach the desired humidity range, between 2.5-3.5%.

Calibration and external phase

After drying, granulate was calibrated in a benchtop granulator at 300 RPM speed through a 1.0 mm mesh sieve. The preparation of the external phase was carried out in a benchtop mixer (Bin Mixer SaintyCo). The granulate was added to the Bin, followed by the inputs, except for magnesium stearate and colloidal silicon dioxide, previously sieved manually in a 1.0 mm mesh sieve. The mixing took place for 10 min at 8 RPM. Afterward, the lubricants sieved in a sieve with 0.5 mm mesh were added, mixing for 3 min at 8 RPM.

Compression process

The tablet compression took place in the Fette 102i tablet press machine using a rotor with 8 punches of 17 x 7.5 mm. The stage was started by adjusting the average tablet weight to 770 mg±5% and compression speed at 63 RPM. For each condition indicated in table 1, all tablets formed within one minute were collected. The average weight was adjusted only at the beginning of the process; the compression parameters were adjusted independently and with the equipment stopped for each variable.

Analysis of quality attributes

Tests chosen to assess the impact of the compression parameters were all carried out based on the one described in the general methods of the Brazilian Pharmacopoeia [22].

Friability

Friability analysis was executed with the weighing of 10 tablets by submitting them to the Erweka TAR 120/220 friabilometer for 4 min at 25 RPM.

Disintegration time

An Erweka ZT 320 disintegrator was used for this test. The water used as the immersion liquid was kept at 37±1 °C. Was used 6 pills in each vat and the time was recorded as soon as the last pill was completely disintegrated. The established time limit was 30 min.

Hardness and relative hardness variation

This test was performed with an Erweka durometer model THB 125. The mean and the relative amplitude, calculated by the difference of the minimum and maximum hardness of 10 tablets was determined, in addition to the calculation of the relative standard deviation.

Average weight and weight variation

Were weighed 20 tablets, individually on the scale (Metler Toledo-AL204) with subsequent calculation of the standard deviation. The specification recommended by the Pharmacopoeia is a variation of ±10% in relation to the ideal average weight.

RESULTS AND DISCUSSION

Table 2 shows the order of the experiments as well as the results obtained for each response variable. Analyzing the results, one can affirm that, by the programmed compression parameters, was

observed that there was an influence on the disintegration time. However, it was not possible the statistical correlation with the programmed parameters, a fact that was confirmed by the non-significance of the model, indicated by the p-value greater than 0.05. In this test, the evaluated tablets took an average of 395 s for complete disintegration, with values of a minimum of 309 s and a maximum of 456 s. Such results are within the recommended by the Brazilian Pharmacopoeia, which specifies that the tablets should not

take more than 1800 s to disintegrate [22]. The model's non-significance was attributed mainly to two factors. First, the presence of sodium lauryl sulfate in the formulation, which has the function of increasing the active ingredient wettability, which in turn can lead to a lower disintegration time regardless of the hardness obtained. Second, the pre-compression and main compression force ranges may not have been wide enough to demonstrate a significant variation in the test [23].

Table 2: Complete factorial experimental design with 3 factors in 2 levels with 3 central points, as well as the results obtained for each response variable

Run	MCF (kN)	SFOM (RPM)	PCF (kN)	DES (s)	RHV (%)	FRI (%)	HAR (kp)	WV (mg)
1	6.5	40	3.79	369	0.169919	0.012	9.6	17.7291
2	10	55	5.615	371	0.183783	0.049	15.6	17.99386
3	3	25	5.615	456	0.30786	0.179	6.8	17.06729
4	10	25	5.615	385	0.154417	0.01	15.35	22.42497
5	6.5	40	3.79	427	0.191025	0.115	11.25	18.11983
6	6.5	40	3.79	385	0.226189	0.095	11.25	18.56584
7	3	55	1.965	427	0.12859	0.918	4.55	12.77506
8	10	55	1.965	397	0.084606	0	16	10.49255
9	3	25	1.965	309	0.278909	1.05	4.5	26.74043
10	10	25	1.965	364	0.239973	0.075	14.8	20.03285
11	3	55	5.615	452	0.135194	0.007	7.2	11.06578

MCF = Main Compression Force, SFOM = FOM Speed, PCF = Pre-Compression Force, DES = Disintegration Time, RHV = Relative Hardness Variation, FRI = Friability, HAR = Hardness, WV = Weight Variation.

The Friability response variable was impacted when the compression and pre-compression force parameters were changed. However, it was not possible to establish a statistical model to correlate the effects with the responses, since the p-value was above 0.05. According to Masilungan and Kraus (1989), the correlation between strength parameters and friability is explicit, indicating the role of increasing hardness, to a certain extent, in decreasing friability [24].

Looking at table 2, it is possible to argue that, at least empirically, when the main compression force of 10 kN is exerted, the highest tested force, the average friability results are about 15 times lower when compared to that obtained using the lowest force, 3 kN. It is still possible to correlate the pre-compression force, because when

applied at its highest tested value, 5.615 kN, there is also a positive impact on the friability values.

The Weight Variation variable (WV), on the other hand, was directly impacted by the Fill-O-Matic Speed factor (SFOM) and by the interaction of Fill-O-Matic Speed, Main Compression Force, and Pre-Compression Force factors.

The data obtained through the analysis of variance (table 3) for the Weight Variation attribute showed normal behavior, the residues are distributed randomly around zero and there are no outliers. The values are arranged within the acceptable range (3σ to -3σ). The p-value of the model at 0.0020 and the F-value 83.28, as well as the non-significance of the Lack of Fit, indicate the significance for a linear model.

Table 3: Analysis of variance (ANOVA) of the response variables, adopting a 95% confidence level

Hardness (kp)	SS	DF	MS	F Value	P-value prob>F	S
Model	187.21125	1	187.21125	170.604	<0.0001	significant
A-Main Compression	187.21125	1	187.21125	170.604	<0.0001	
Curvature	0.021818182	1	0.021818182	0.019883	0.8914	not significant
Residual	8.77875	8	1.09734375			
Lack of Fit	6.96375	6	1.160625	1.278926	0.5008	not significant
Pure Error	1.815	2	0.9075			
Cor Total	196.0118182	10				
Relative hardness variation (%)						
Model	0.025198653	1	0.025198653	10.1339	0.0129	significant
B-FOM Speed	0.025198653	1	0.025198653	10.1339	0.0129	
Curvature	9.3453E-05	1	9.3453E-05	0.037583	0.8511	not significant
Residual	0.019892563	8	0.00248657			
Lack of Fit	0.018276507	6	0.003046084	3.769777	0.2245	not significant
Pure Error	0.001616056	2	0.000808028			
Cor Total	0.045184669	10				
Weight variation (mg)						
Model	228.0499	6	38.00832	83.27746	0.0020	significant
A-Main Compression	1.357678	1	1.357678	2.974716	0.1830	
B-FOM Speed	143.9761	1	143.9761	315.4562	0.0004	
C-Pre-compression	0.277136	1	0.277136	0.607215	0.4927	
AB	4.493217	1	4.493217	9.844783	0.0518	
AC	56.58272	1	56.58272	123.9745	0.0016	
BC	21.36312	1	21.36312	46.80728	0.0064	
Curvature	1.446227	1	1.446227	3.168729	0.1731	not significant
Residual	1.369217	3	0.456406			
Lack of Fit	1.018638	1	1.018638	5.811164	0.1375	not significant
Pure Error	0.35058	2	0.17529			
Cor Total	230.8654	10				

SS = Sum of Squares, DF = Degree of Freedom, MS = Mean Square, S = Significant

In fig. 1, the effect of changing the Fill-O-Matic Speed and Pre-Compression force parameters on the Weight Variation response variable is demonstrated. The influence of FOM Speed on weight variation has already been mentioned in the literature. Some studies correlate the significance of this influence with the flow characteristics of the powder [25]. Free-flowing powders do not have a significant impact of the FOM Speed on quality attributes; however, for powders with less flow, the use of different speeds directly impacts quality attributes [26]. The drug chosen as a model for this study, Albendazole 400 mg, has the characteristic of a fine

powder, even after granulation, since the active ingredient is micronized and is present in a large percentage in the formulation. Even not determining the flow properties, it is possible, visually, to assume that the material does not have a good/excellent flow.

The model also indicated interactions between the Main Compression Force and Pre-Compression Force. When increasing the Main Compression Force, the Weight Variation increases when 5.615 kN of Pre-Compression force is applied. However, when the Pre-Compression force was 1.965 kN the opposite effect was observed.

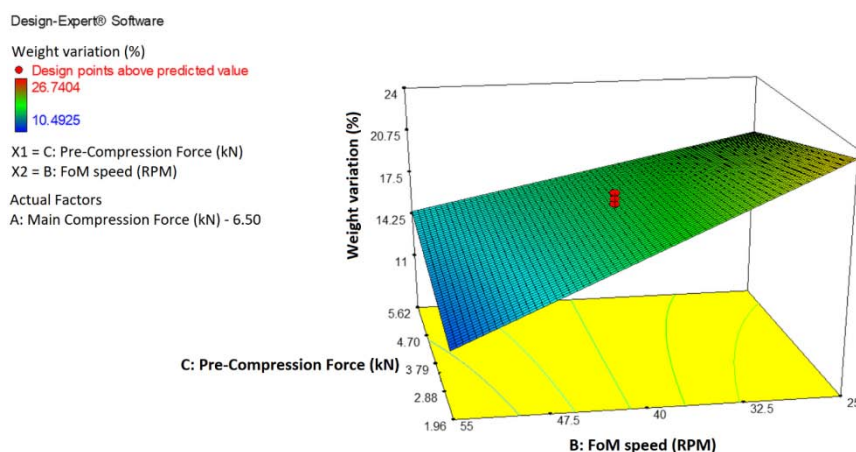


Fig. 1: Impact of changing the FOM speed factor on the response to weight variation

The interactions of other factors, such as the FOM Speed with the Pre-Compression force, do have an impact on the Weight Variation response variable, but they will not be considered in this discussion, due to the small influence they have on the effect, only 8.59% of the total. However, for the significance of the model, these factors were considered, as shown in the equation below.

$$\text{Weight variation} = 51.276 - 2.031\text{MCF} - 0.602\text{SFOM} - 5.196\text{PCF} + 0.0142(\text{MCF})(\text{SFOM}) + 0.416(\text{MCF})(\text{PCF}) + 0.059(\text{SFOM})(\text{MCF})$$

where: MCF = Main Compression Force, PCF = Pre-Compression Force e SFOM = Fill-O-Matic Speed.

The variables of Hardness and Relative Hardness Variation were impacted by the Main Compression values chosen for the experimental design.

Hardness was impacted by the change in the Main Compression Force, having a positive effect; that is, according to the increase in the main compression force, the data obtained by the experiment (fig. 2) showed normal behavior. The residues are randomly distributed around from zero and there are also no outliers with values within the acceptable range (3σ to -3σ). The p-value of the model at 0.0001 and the F-value of 170.60, as well as the non-significance of the Lack of Fit, indicate the significance for a linear model.

It is possible to indicate the appropriate force range to comply with the specifications outlined in table 1. According to fig. 2, the force specification range should be between 6 to 9 kN in the Main Compression Force and, regardless of the force exerted in the pre-compression phase, the resulting Hardness will be between 9-15 kp according to the model. This behavior is already easily found in the literature, where the greater the main compression force employed, the greater the resulting hardness. However, there is a breaking point where the tablet cannot increase the hardness any more regardless of the force used [27].

The equation that was provided by the model was represented below:

$$\text{Hardness} = 1.616 + 1.382\text{MCP}$$

where: MCF = Main Compression Force.

Regarding the hardness variation, expressed by the Relative Hardness Variation response of each 20 tablets, it was possible during data analysis (table 3) to determine the negative relationship of the FOM Speed (fig. 2) in the hardness variation values. The higher the FOM Speed, the smaller the observed Hardness Variation, according to the model equation shown below.

$$\text{Hardness Variation} = 0.339 - 3.741 \times 10^{-3} \text{SFOM}$$

where: SFOM = Fill-O-Matic Speed.

The data obtained showed normality and random distribution around the zero axes, the residues remained within the expected range of 3 to -3 standard deviations, added to the p-value of the model 0.0129 and the non-significance of the Lack of Fit, we assume that the model built is significant.

As can be seen from fig. 2, the FOM Speed significantly impacts the Relative Hardness Variation found. It can be established, therefore, that the 55 RPM FOM Speed is ideal within the values tested for the speed of 63 RPM of the tablet press rotor, since it presented lower values of weight variation as well as in hardness.

After all the experiments, it can be seen that regardless of the factors used, the Disintegration Time and Friability remained within that specified in table 1. This way, the ranges used in this investigation can be applied during batch production. However, as already discussed, the variables Hardness, Relative Hardness Variation, and Weight Variation are impacted by the factors of Main Compression Force and/or FOM Speed.

At the end of this study, it can be verified that the ranges of the factors Main Compression Force of 6 to 9 kN, Pre-Compression Force of 1,965 to 5,615 kN, and 55 RPM of FOM Speed, are responsible for all the attributes of analyzed qualities to remain within the specification expected. Comparing with other authors who carried out a similar investigation in the compression stage [12], it is observed that our study found some different results, mainly in the responses of Friability and Disintegration Time. As briefly discussed earlier, the force ranges used in this work, added to the intrinsic characteristics of our formulation, may have led to the behavior observed.

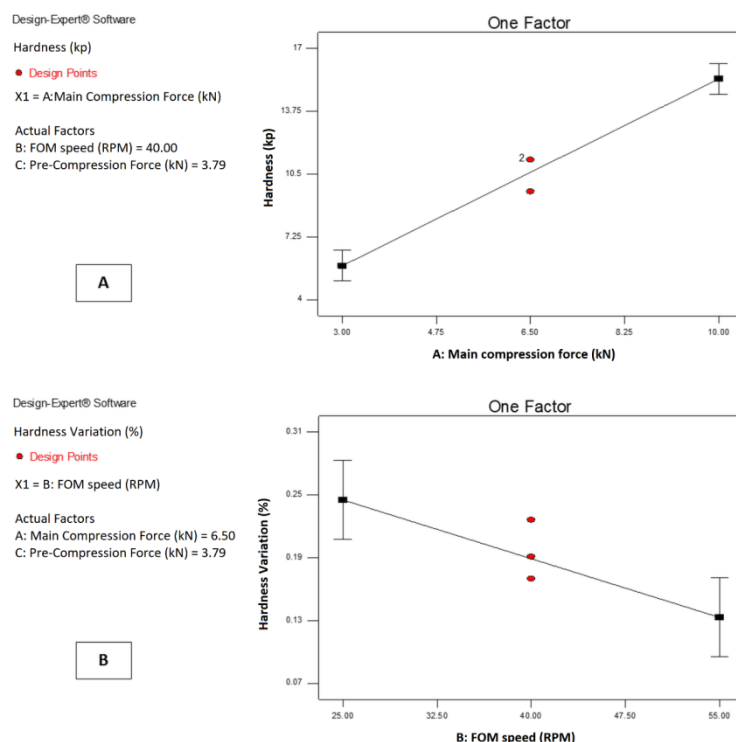


Fig. 2: Effects observed by changing the parameters of the main compression force and FOM speed, in hardness (A) and relative hardness variation (B)

CONCLUSION

The results of this investigation show that it was possible to apply the Design of Experiment (DoE) methodology in the compression process of the drug Albendazole 400 mg and to assess the impact of the parameters on this tablet production phase. Such knowledge was fundamental for a better understanding of the intrinsic characteristics of our formulation as well as the equipment used. This study showed that the values of the parameters Main Compression Force between 6 to 9 kN, Pre-Compression Force from 1.965 to 5.615 kN, and 55 RPM of FOM Speed at a compression speed set at 63 RPM, config. a safe and reliable working range for routine production of the product studied, in addition to significantly increasing the productivity since the usual speed of production is about 6 times lower than that tested in this article. The FOM Speed parameter was the main control factor to maintain quality attributes. In a future investigation, the use of alternative tablet press speed ranges and FOM speeds can be studied in order to further optimize the production process.

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Nil

AUTHORS CONTRIBUTIONS

Lucas da Silva performed experiments, analyzed data, and co-wrote the paper. Emerson Boldo supervised the research and co-wrote the paper.

CONFLICT OF INTERESTS

The authors declare that there are no conflicts of interest regarding the publication of the paper.

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